Journal of Mining and Metallurgy 43 B (2) (2007) 161 - 169

Journal of Mining and Metallurgy

## PHASE RELATIONS NEAR TERNARY EUTECTIC POINT IN THE Ag-In-Sb SYSTEM

## D. Jendrzejczyk-Handzlik<sup>\*#</sup>, D. Živković<sup>\*\*</sup>, W. Gierlotka<sup>\*</sup>, D. Manasijević<sup>\*\*</sup>, K. Fitzner<sup>\*</sup> and D. Minić<sup>\*\*\*</sup>

 \* AGH University of Science and Technology, Faculty of Non-Ferrous Metals, Laboratory of Physical Chemistry and Electrochemistry, 30-057 Kraków, Poland
\*\* University of Belgrade, Technical Faculty Bor, Dept. of Metallurgy and Material Engineering, 19210 Bor, Serbia
\*\*\* University of Priština, Faculty of Technical Sciences, 38220 Kosovska Mitrovica, Serbia

(Received 10 September 2007; accepted 19 October 2007)

## Abstract

The results of the phase relations near ternary eutectic point in the Ag-In-Sb system are investigated in this paper. Phase equilibrium calculation was done using Thermocalc software and experimental DTA results for the chosen alloys in the isopleths with molar ration of In:Sb = 7:3; 9:1 and 1:1. The structural characteristics of these alloys have been investigated using light optic microscopy and scanning electron microscopy, while hardness measurements have also been done. Solidification path for three ternary alloys located on three different investigated isopleths was calculated using Pandat software.

Keywords: lead-free solders, phase equilibria, ternary systems, Ag-In-Sb alloys

### 1. Introduction

A need for a substitution of conventional lead-bearing solders stimulated widespread search for new lead-free materials, which can be used in automotive, avionics and electronic industry. As a response to NCSM Lead-Free Soldering Project in the United States [1] as well as JEIDA and JWES projects carried out in Japan [2], European Union created COST 531 Action, which main aim was to choose possible candidates for lead-free solders among several groups of alloys. It was soon established that the group of silver-based alloys with the additions of low-melting metals like Sn, Bi or In can be a

<sup>&</sup>lt;sup>#</sup>Corresponding author: djendrze@uci.agh.edu.pl

DOI:10.2298/JMMB0702161J

good substitute for idustrial application. However, to adjust solidification temperature as well as the structure and mechanical properties of the joint, a wide range of other metals can be introduced into the alloy as a third component.

Investigations of antimony addition to Ag-In system has been recently carried out by Buchtova et al. [3] and Živković et al. [4,5] Isothermal section of this system at 200<sup>o</sup> C was experimentally determined, as well as the isophlet for the ratio of In : Sb =1. In order to find out how the antimony addition will influence the temperature of the eutectic point in the binary Ag-In system and how phase relations after this addition may look like, the particular part of the ternary system with low Sb content was investigated in this work. Next, using previously optimized parameters [6] these results were compared with the phase relations derived from computer calculations.

### 2. Experimental procedure

The samples, of chosen alloys along the investigated sections with molar ratio of In:Sb equal to 7:3, 9:1 (the compositions and masses are presented in Table 1) and 1:1 (sample with 10, 20 and 40 wt%Ag), were prepared from Ag, In and Sb of 99.99% purity. The samples were prepared in an induction furnace under inert gas atmosphere, where an extra amount of antimony (about 2-3%) was added to compensate the weight loss due to the volatilization of antimony.

Differential thermal analysis (DTA) was performed using Derivatograph (MOM, Budapest). The experiments were carried out with the heating rate  $10^{\text{ O}/\text{min}}$ , using sintered Al<sub>2</sub>O<sub>3</sub> as the reference specimen.

Light optic microscopy was performed at Reichert  $MeF_2$  microscope, using concentrated  $H_2O_2$  or solution of  $(32gFeCl_3+100mlH_2O_2+100mlH_2O)$  as etching reagents, while scanning electron microscopy (SEM) was Performed at JEOL/JSM T20 scanning microscope.

X-ray diffraction (XRD) analysis was carried out using X-ray diffractometer (Siemens), with Cu anticathode and Ni filters ( $2\theta$  in range 4-68, intensity in range from 0-600/800).

Standard apparatus for Vickers hardness measurements was used in this kind of experiments.

## 3. Results and Discussion 3.1. Phase equilibrium determination

Differential thermal analysis (DTA) was performed on samples along two isophlets determined by In:Sb ratio 9:1 and 7:3, respectively, and the obtained results are gathered in Table 2. The evolution of phase equilibria with antimony addition, starting from binary Ag-In system (Fig.1a), is shown in subsequent Figures 1a through 1d. In Figure 1d the isophlet for the ratio In:Sb =1:1, determined previously [3,4], is also for comparison. The results shown demonstrate the change of the position of the eutectic point with the increase of antimony content.

The Ag-In-Sb system consists of the following phases [7]: FCC\_A1 - solid solution based on silver, HCP\_A3 - which continuously exists from the Ag-In side to the Ag-Sb side in the ternary Ag-In-Sb system, ZINCBLENDE\_B3 - phase based on In and Sb as the main constituents in almost equiatomic composition,

Table 1. The composition and masses of chosen alloys in the investigated sections with molar ratio of In:Sb equal to 7:3 (a) and 9:1 (b)

| Section with molar ratio In:Sb=7:3 |      |      |         |         |         |                |
|------------------------------------|------|------|---------|---------|---------|----------------|
| xAg                                | xIn  | xSb  | wt%Ag   | wt%In   | wt%Sb   | sample mass, g |
| 0,1                                | 0,63 | 0,27 | 9,2993  | 62,3613 | 28,3394 | 2,1971         |
| 0,2                                | 0,56 | 0,24 | 18,7445 | 55,8673 | 25,3882 | 2,2686         |
| 0,3                                | 0,49 | 0,21 | 28,3392 | 49,2705 | 22,3904 | 2,3461         |
| 0,4                                | 0,42 | 0,18 | 38,0868 | 42,5685 | 19,3447 | 2,4305         |
| 0,5                                | 0,35 | 0,15 | 47,9910 | 35,7588 | 16,2502 | 2,5226         |
| 0,6                                | 0,28 | 0,12 | 58,0558 | 28,8388 | 13,1054 | 2,6238         |
| b)                                 |      |      |         |         |         |                |

| Section with molar ratio In:Sb=9:1 |      |      |         |         |        |                |
|------------------------------------|------|------|---------|---------|--------|----------------|
| xAg                                | xIn  | xSb  | wt%Ag   | wt%In   | wt%Sb  | sample mass, g |
| 0,1                                | 0,81 | 0,09 | 9,4004  | 81,051  | 9,5491 | 2,2378         |
| 0,2                                | 0,72 | 0,08 | 18,9269 | 72,528  | 8,5451 | 2,3080         |
| 0,3                                | 0,63 | 0,07 | 28,5820 | 63,891  | 7,5274 | 2,3839         |
| 0,4                                | 0,54 | 0,06 | 38,3684 | 55,1357 | 6,4959 | 2,4661         |
| 0,5                                | 0,45 | 0,05 | 48,2888 | 46,2609 | 5,4503 | 2,5554         |
| 0,6                                | 0,36 | 0,04 | 58,3459 | 37,2638 | 4,3903 | 2,6528         |

TETRAGONAL\_A6 - phase based on indium, RHOMBOEDRAL\_A7 - phase based on antimony, AGSB\_ORTHO - phase based on silver and antimony, intermediate stoichiometric compounds Ag<sub>2</sub>In and AgIn<sub>2</sub>, and the liquid phase.

Using the thermodynamic description of the ternary system, which was worked out in our earlier paper [6], the respective isopleths were calculated using ThermoCalc software and were compared with the experimental DTA results, as shown in Figures 1a - 1d.

It was found that the calculated ternary eutectic point occurs at temperature of 414,9K at the composition equal to  $X_{Ag} = 0,014$  and  $X_{Sb} = 0,017$  mole fractions. So, isothermal sections just above and below ternary eutectic temperature were calculated using Pandat [8] software and are shown in Fig.2a and 2b.

The existence of calculated ternary eutectic checked point has been experimentally, using DTA and metallography, as shown in Fig.3. The eutectic structure was proven and the eutectic temperature of 419.5K (or 146.5°C) was obtained, which is in accordance with the value predicted by calculation. Also, this is in agreement with literature data presented in [9], in which the ternary eutectic in the Ag-In-Sb system is given at the temperature of 417K (or 144<sup>o</sup>C).

# **3.2.** Structural characteristics of the alloys

In order to find out how the solidification process of the alloy may depend on antimony addition, some of the alloys in the investigated sections were investigated using

| Alloy                   | Results of measurments | H <sub>v</sub> average |
|-------------------------|------------------------|------------------------|
| 10wt%Ag                 | 101, 102, 103          | 102                    |
| (molar ratio In:Sb=1:1) |                        |                        |
| 20wt%Ag                 | 117, 118, 119          | 118                    |
| (molar ratio In:Sb=1:1) |                        |                        |
| 40wt%Ag                 | 133, 140               | 137                    |
| (molar ratio In:Sb=1:1) |                        |                        |
| 50wt%Ag                 | 109, 109, 110          | 109                    |
| (molar ratio In:Sb=7:3) |                        |                        |
| 40wt%Ag                 | 165, 145               | 155                    |
| (molar ratio In:Sb=9:1) |                        |                        |

Table 2. DTA results obtained for investigated sections in the Ag-In-Sb system



Fig. 1. Binary Ag-In system (a); Isopleth for  $X_{In}/X_{Sb}=9:1$  (b); Isopleth for  $X_{In}/X_{Sb}=7:3$  (c); Isopleth for  $X_{In}/X_{Sb}=1:1$  (d)



Fig.2. a) Isothermal section of the ternary system at T = 420 K; b) Isothermal section of the ternary system at T = 414 K

light optic microscopy (Fig.4), scanning electron microscopy (Fig.5) and X-ray diffraction analysis (Table 3).

Reasonable agreement between the experimental data (LOM, SEM and XRD) and the results of calculations in the field near ternary eutectic point in the In-rich part of the investigated system was found.

# **3.3.** Calculation of the solidification path

Solidification path for three ternary alloys located on three different isophlets, and investigated by metallographic and SEM



methods was calculated using Pandat software [8]. Scheil model of the alloy solidification was used during these calculations. The obtained results for three different solidification paths are shown in Fig.6. Depending on In/Sb ratio different three-phase equilibrium is obtained at the end of the solidification process, which is in accordance to obtained experimental data.

### 3.4. Hardness measurements

Hardness tests of alloys chosen from three different investigated isopleths were



Fig.3. DTA (a) and microphotograph (b) of the ternary eutectic point



Fig.4. The results of light optic microscopy for the samples with (a) 10wt%Ag (section In:Sb = 1:1) and (b) 40 wt%Ag (section In:Sb = 9:1) Magnification: x150 (a); x300 (b)

performed with standard apparatus used for Vickers hardness measurements. The results, gathered in Table 4, are shown in Fig.7 for the section with In:Sb molar ratio equal to 1:1. Most probably, the increasing amount of HCP\_A3 phase influence the increase of the hardness of the alloys. Also, the presence of the intermetallic phases may either decrease



 $(AgIn_2)$  or increase  $(Ag_2In)$  the hardness of the alloy.

## 4. Conclusions

This paper deals with the investigations of the phase relations near ternary eutectic point in the Ag-In-Sb system, which can be a potential lead-free solder.



Fig.5. The results of scanning electron microscopy for the samples with: (a) 10wt%Ag (section In:Sb = 1:1), (b) 50wt%Ag (section In:Sb = 7:3) and (c) 40wt%Ag (section In:Sb = 9:1) Magnification: x2000 (a); x3500 (b); x1000 (c)

Table 3. The results of X-ray diffraction analysis for the samples with 10wt%Ag (section In:Sb = 1:1), 50wt%Ag (section In:Sb = 7:3) and 40wt%aAg (section In:Sb = 9:1)

| 10%wtAg (In:Sb=1:1) |              |  |  |
|---------------------|--------------|--|--|
| (nm)                |              |  |  |
| 0.3253              |              |  |  |
| 0.3116              | In-Sb        |  |  |
| 0.2586              | Ag-In, Ag-Sb |  |  |
| 0.2404              | Ag-In, Ag-Sb |  |  |
| 0.2277              | Ag-In, Ag-Sb |  |  |
| 0.2146              | In-Sb        |  |  |
| 0.1869              | In-Sb        |  |  |
| 0.1762              | Ag-In, Ag-Sb |  |  |
| 0.1490              | Ag-In, Ag-Sb |  |  |
| 0.1409              | In-Sb        |  |  |
| 0.1362              | Ag-In, Ag-Sb |  |  |

~)

h)

|        | 0)              |    |
|--------|-----------------|----|
| 50wt   | %Ag (In:Sb=7:3) |    |
| (nm)   |                 | (1 |
| 0.3769 |                 | 0. |
| 0.3563 |                 | 0. |
| 0.3112 | In-Sb           | 0. |
| 0.2712 |                 | 0. |
| 0.2598 | Ag-Sb           | 0. |
| 0.2402 | Ag-In, Ag-Sb    | 0. |
| 0.2283 | Ag-Sb           | 0. |
| 0.2147 | In-Sb           | 0. |
| 0.1762 | Ag-In, Ag-Sb    | 0. |
| 0.1654 |                 | 0. |
| 0.1496 | Ag-Sb           | 0. |
| 0.1411 | In-Sb           |    |
| 0.1363 | Ag-In, Ag-Sb    |    |

c) 40%Ag (In:Sb=9:1) nm) 3762 3568 Ag-In 3130 (In) 2708 2603 Ag-In 2343 Ag-In 2239 (In) 2156 1655 Ag-In 1412 Ag-In 1353 (In)







Fig.6. The obtained results for three calculated solidification paths of chosen alloys: (a) equilibrium -scheil model; (b) scheil model; (c) - scheil model

experimental In the frame of determination, DTA, LOM, SEM and hardness measurement were performed. Based on these results and the results of calculations, phase equilibrium for the isopleths with molar ration of In:Sb = 7:3;

| Alloy                   | Results of measurments | H <sub>v</sub> average |
|-------------------------|------------------------|------------------------|
| 10wt%Ag                 | 101, 102, 103          | 102                    |
| (molar ratio In:Sb=1:1) |                        |                        |
| 20wt%Ag                 | 117, 118, 119          | 118                    |
| (molar ratio In:Sb=1:1) |                        |                        |
| 40wt%Ag                 | 133, 140               | 137                    |
| (molar ratio In:Sb=1:1) |                        |                        |
| 50wt%Ag                 | 109, 109, 110          | 109                    |
| (molar ratio In:Sb=7:3) |                        |                        |
| 40wt%Ag                 | 165, 145               | 155                    |
| (molar ratio In:Sb=9:1) |                        |                        |

Table 4. The results of hardness measurements



Fig.7. Dependence of hardness on composition for the alloys in section with molar ratio In:Sb=1:1

9:1 and 1:1 was determined. The calculated ternary eutectic point was obtained at temperature of 414,9K and its composition is equal to  $X_{Ag} = 0,014$  and  $X_{Sb} = 0,017$ . The ternary eutectic is formed during the reaction, which taken place when three tie triangles: (tetragonal A6-L-AgIn<sub>2</sub>), (AgIn<sub>2</sub>-L-Zincblende B3) and (Zincblende B3-L tetragonal A6) descending from higher temperature meet at four-phase plane at eutectic temperature. Then, only one tie-triangle (tetragonal A6-Ag<sub>2</sub>In-Zincblende B3) is descending from the four phase plane to lower temperature. The respected solidification path's for three ternary alloys

located on three different investigated isopleths are also shown.

#### Acknowledgement

The authors from Serbia are thankful to the Ministry of Science of Republic of Serbia for the financial support under the project  $N^0$ 142043. Presented investigations have been realized in the frame of COST531 Action.

The authors from Poland are thankful to the State Committee for Scientific Research and AGH University of Science Technology, Faculty of Non - Ferrous Metals under fund number 11.11.180.125 and under COST 531 Action no. 112/E-356/SPB/COST/T-08/DWM 571 /2003-2006.

#### References

1. F.W. Gayle, G. Becka, J. Badgett, G. Whitten, T.Y. Pan, A. Grusd, B. Bauer, R. Lathrop, J. Slattery, I. Anderson, J. Foley, A. Gickler, D. Napp, J. Mather, Ch. Olson, *JOM* (2001) 17

2. ESPEC Technology Report, No13 (2002) 1.

3. V.Buchtova, D.Živković, J.Vreštal, D.Manasijević, A.Kroupa, *Monatshefte fur Chemie*, 136 (2005) 1939.

4. D.Živković, D.Manasijević, Ž.Kamberović, M.Cocić, B.Marjanović, Metalurgija (*Metallurgy*), 46 (2007) 151.

5. D.Živković, D.Manasijević, I.Mihajlović, Ž. Živković, *Journal of Serbian Chemical Society*, 71 (3) (2006) 203-211.

6. D.Jendrzejczyk, W.Gierlotka, K.Fitzner, *Zeitschrift für Metallkde*, 97 (2006) 1519.

7. A.T. Dinsdale, A. Kroupa, J. V'Izdal, J. Vrestal, A. Watson, A. Zemanova, COST 531 Database for Lead-free Solders, Version 2.0, 2006.

8. Pandat , CompuTherm. LLC 437 Yellowstone Dr, Suite 217, Madison, WI 53719 USA

9. X.J.Liu, T.Yamaki, I.Ohnuma, R.Kainuma, K.Ishida, *Mater.Trans. JIM*, 45 (3) (2004) 637.